### A 3D METHOD FOR PROFILING THE SHAPING TOOL FOR THE GENERATION OF HELICAL SURFACES

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### ABSTRACT

It is proposed a graphical method for profiling the shaping tool used to generate cylindrical helical surface with constant pitch. The method, developed in the CATIA graphical design environment, is based on the helical movement decomposition into an assembly of equivalent movements, rotation and translation.

A dedicated software application allows for modeling of the helical surface, determining the characteristic curve and the crossing section of the cylindrical surface, reciprocally enveloping with the helical surface. These are presented applications for the generation of helical surface as trapezoidal thread and ball thread.

KEYWORDS: helical surface, cylindrical surface, shaping tool

### 1. Introduction

The cylindrical helical surfaces with constant pitch are frequently used in the construction of machine parts which transmit movements (helical teethed wheels, translation screws) or which circulate fluids under pressure (helical pumps, helical compressors). The generation of the helical surfaces is made using tools bounded by surfaces of revolution — the case of side mill, in some other cases, when the helical flute has symmetrical flanks, are used end mill tools [1], [7].

For the situation when the machining technology requires the construction of a simple tool (usually with a single cutting edge), as example for the prototypes machining or for repairs, it is possible to use for the generation of a complex helical surface, profiled shaping tools [1], [2], [3], [6].

The shaping tools profiling, tools which in the cutting motion (alternative rectilinear) generate a cylindrical surface, requires the determination of the condition that this surface should be reciprocally enveloping with the cylindrical helical surface with constant pitch.

There are known analytical methods for the determination of a cylindrical surface reciprocally enveloping with a helical surface: 1st Olivier's theorem (the contact between the two surfaces is a contact of first degree, [2], [4]), Gohman's theorem [2], the method of helical movement decomposition — Nikolaev's condition [2], [4].

Also, there may be used specific theorems of the "minimum distance method" [5], as well as, of the "in-plane generating trajectories" [6].

As well, there are known graphical methods for profiling the generating tool for a cylindrical surface, developed in AutoCAD, based on the principle of solid body intersection [1].

In this paper, is presented a way to profile a cylindrical surface, reciprocally enveloping with a cylindrical helical surface with constant pitch, based on the capabilities of the CATIA design environment, method which allows for the graphical determination of the characteristic curve and the crossing section of the cylindrical surface, section which represents the profile of the shaping tool.

The method is rigorous, intuitive and easy to apply, based on a dedicated software, elaborated in *Visual Basic Application*.

# 2. Generation kinematics using the shaping tool

The generation of the helical surface with shaping tool is a manufacturing possibility used for a prototype machining or for reparations, the machining productivity being relatively low.

The tool, usually a profiled cutting tool, executing an alternative rectilinear movement, with a single cutting travel stroke, generates a cylindrical surface, which is reciprocally enveloping with the helical surface to be generated.

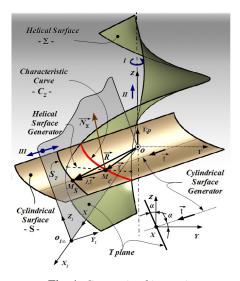


Fig. 1. Generation kinematics

The minimum kinematics of the process, Figure 1, supposes the movements:

*I* and *II* are rotation and translation movements, around and along the helical surface axis, usually uniform motions, generating a helix with axis and helical parameter identical with those of the surface to be generated;

*III* — alternative rectilinear tool's motion. In this motion, the cutting edge generate the cylindrical surface.

The contact curve between the cylindrical surface and the helical one represents the geometrical locus of the points, belonging to the helical surface, where the two surfaces are tangent. This represents the characteristic curve of the helical surface in movement along the cylindrical surface generatrix.

For a helical surface, in principle in the form:

$$\begin{aligned}
X &= X(u,v); \\
\Sigma &= Y(u,v); \\
Z &= Z(u,v),
\end{aligned}$$
(1)

defined in the *XYZ* reference system, with u and v independent variable parameters, and a direction of the generatrix of the generating cylindrical surface,

$$\vec{t} = -\cos\alpha \cdot \vec{j} - \sin\alpha \cdot \vec{k} , \qquad (2)$$

is defined the specific enveloping condition,

$$\vec{N}_{\Sigma} \cdot \vec{t} = 0.$$
 (3)

In the equation (3), the normal at the surface  $\Sigma$  is

$$N_{\Sigma} = N_X \cdot i + N_Y \cdot j + N_Z \cdot k. \tag{4}$$

In this way, the condition for the determination of the characteristic curve becomes, see (2) and (4),

$$V_Y \cdot \cos \alpha + N_Z \cdot \sin \alpha = 0, \qquad (5)$$

 $N_{Y} \cdot \cos \alpha + \lambda$  equivalent to dependency,

$$v = v(u) . \tag{6}$$

The assembly of the equations (1) and (6) represents the characteristic curve onto the cylindrical helical surface on type, see Figure 1:

$$C_{\Sigma} \begin{vmatrix} X = X(u); \\ Y = Y(u); \\ Z = Z(u). \end{cases}$$
(7)

The (7) curve represents a directrix curve of the cylindrical helical surface — surface generated by the cutting edge of the shaping tool.

#### Crossing section of the cylindrical surface

The characteristic curve (7) is a spatial curve and, as follows, is difficult to be used in the practice of the cutting tool's machining as a major cutting edge, due to the difficulties to measure this kind of curves.

It is accepted as the simplest solution to materialize the cutting edge of the shaping tool by the crossing section of the cylindrical surface (the section with a plane which contains the X axis and is perpendicular to the versor of the cylindrical surface, see Figure 1.

In this way, the cylindrical surface is described by:

$$\vec{R} = \vec{r} + \lambda \cdot \vec{t} , \qquad (8)$$

with  $\lambda$  arbitrary parameter and *r* the versor of the current point from the characteristic curve, see (7), or in analytical form:

$$X = X(u);$$
  

$$S | Y = Y(u) - \lambda \cdot \cos \alpha;$$
  

$$Z = Z(u) - \lambda \cdot \sin \alpha.$$
(9)

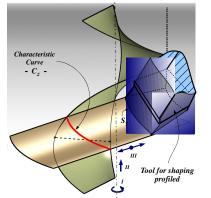


Fig. 2. The characteristic curve and the shaping tool

The section of the *S* surface with the plane *T*, plane which contains the X axis and is normal to  $\vec{t}$ ,

 $Y \cdot \cos \alpha + Z \cdot \sin \alpha = 0, \qquad (10)$ 

leads to the determination of the crossing section  $S_T$ , in principle, see (9), in the form:

$$S_{T} \begin{vmatrix} X = X(\lambda); \\ Y = Y(\lambda); \\ Z = Z(\lambda). \end{cases}$$
(11)

The *ST* curve — the crossing section — unlike the characteristic curve is an in-plane curve. This thing makes it easy to be used as cutting edge for the cutting tool — the shaping tool, see Figure 2.

# 3. The 3D method for shaping tool profiling

The enveloping condition, (5), is equivalent to a similar condition regarding the generation of the helical surface, by enveloping with a tool bounded by a revolution primary peripheral surface but with an infinite diameter [2].

In this way, if it is accepted that the relative position of a revolution surface, regarding the helical surface should be generated, then the specific enveloping condition is in the form [3], [4]

$$\begin{vmatrix} 0 & -\sin\alpha & \cos\alpha \\ N_X & N_Y & N_Z \\ X(u,v) - a & Y(u,v) & Z(u,v) \end{vmatrix} = 0 \quad (12)$$

which, for  $a \rightarrow \infty$  (the side mill is at infinite distance), is equivalent to (5).

In this way, the cylindrical tool may be regarded as a revolution surface with a very large diameter.

In CATIA design environment, using the specific command from the *Generative Shape Design*, is modeled the helical surface. By command Projection is projected the  $Z_i$  axis of the reference system joined with the side mill, substitute for the cylindrical surface, onto the helical surface, obtaining the characteristic curve.

The primary peripheral surface of cylindrical surface is modeled with the Extrude command. With the Intersection command, is intersected the previously modeled cylindrical surface, obtaining the form of the cutting edge of the shaping tool (see Figures 1 and 2).

All this algorithm was synthesized in a specific application *THSG–VBA* (*Tools for Helical Surfaces Generation*), in order to automate these steps.

# 4. Shaping tool's profiling for generation of a trapezoidal thread

It is proposed the application of the presented methodologies for the determination of the cylindrical tool for the generation of a trapezoidal thread, with the input parameters given in Table 1..

In Figure 3, is presented the 3D model of the helical surface and of the reciprocally enveloping cylindrical surface.

Table 1. Input parameters for the trapezoidal thread

Point	Description	Y	Ζ
	_	[mm]	[mm]
Α	Start point of thread crest	50	20
В	Start point of thread flank	50	0
С	End point for the bottom of thread	40	-10
D	End point for the bottom of thread	40	-20
Е	End point for thread flank	50	-30
Se	Flute helix sense	r	ight
pe	Thread pitch	50	) mm
а	The coord. of the origin (X direction)	1000	000 mm

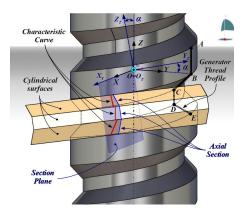


Fig. 3. Primary peripheral surface of the shaping tool

It is obvious that the singular points from the helical surface generatrix generate discontinuities onto the characteristic curve, points  $C_{CC}$ ,  $C'_{CC}$  and  $D_{CC}$ ,  $D'_{CC}$ , see Figure 4.

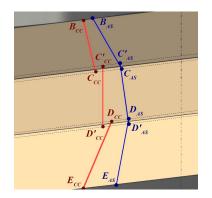


Fig. 4. Composed profile of the crossing section

This makes necessary a modification of the ideal crossing section, with repercussions at the generated profile, see Figure 5.

The axial section was referenced to a translated reference system, with the origin in the point with coordinates  $O_s$  (40, 0, -27.5).

The coordinates of the characteristic curve and of the crossing section of the cylindrical surface are presented in Table 2.

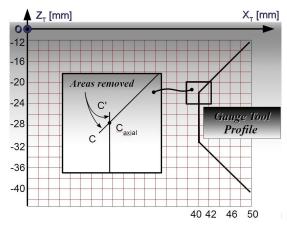


Fig. 5. Axial section of cylindrical tool

**Table 2.** Coordinates of points from the characteristic

 curve and the crossing section of the shaping tool for

 generation of a trapezoidal thread

		X[mm]	Y[mm]	Z[mm]
Characteristic curve		50,0001	-0,0012	-12,5002
		48,8842	-0,1785	-13,6448
	BC	:	:	:
		41,0817	-1,4109	-21,6675
		39,9687	-1,5852	-22,8155
		40,0002	0,0008	-32,4999
		40,0002	0,0008	-31,3888
	CD		÷	:
tct		40,0002	0,0003	-23,6112
arc		40,0002	0,0002	-22,5001
Ch		39,9687	1,5863	-32,1844
•		41,0818	1,4120	-33,3325
	DE	•	•	
		48,8843	0,1801	-41,3551
		50,0003	0,0028	-42,4997
		$X_T$	Y <sub>T</sub>	$Z_T$
		X <sub>T</sub> 50,0001	<i>Y<sub>T</sub></i> 0,0000	Z <sub>T</sub> -12,3447
	BC	50,0001	0,0000	-12,3447
	BC	50,0001	0,0000	-12,3447
	BC	50,0001 48,8840 :	0,0000 0,0000 :	-12,3447 -13,4473
ис	BC	50,0001 48,8840 : 41,0815	0,0000 0,0000 : 0,0000	-12,3447 -13,4473 : -21,1767
ction	BC	50,0001 48,8840 : 41,0815 39,9687	0,0000 0,0000 : 0,0000 0,0000	-12,3447 -13,4473 : -21,1767 -22,2828
ll section	BC CD	50,0001 48,8840  41,0815 39,9687 40,0002	0,0000 0,0000 : 0,0000 0,0000 0,0000	-12,3447 -13,4473 : -21,1767 -22,2828 -22,2204
xial section		50,0001 48,8840  41,0815 39,9687 40,0002	0,0000 0,0000 : 0,0000 0,0000 0,0000	-12,3447 -13,4473 : -21,1767 -22,2828 -22,2204
Axial section		50,0001 48,8840 : 41,0815 39,9687 40,0002 40,0002 :	0,0000 0,0000	-12,3447 -13,4473 : -21,1767 -22,2828 -22,2204 -23,3177 :
Axial section		50,0001 48,8840  41,0815 39,9687 40,0002 40,0002  40,0002	0,0000 0,0000  0,0000 0,0000 0,0000  0,0000  0,0000	-12,3447 -13,4473 : -21,1767 -22,2828 -22,2204 -23,3177 : : -30,9988
Axial section		50,0001 48,8840 : 41,0815 39,9687 40,0002 40,0002 : 40,0002 40,0002	0,0000 0,0000	-12,3447 -13,4473 : -21,1767 -22,2828 -22,2204 -23,3177 : : -30,9988 -32,0961
Axial section		50,0001 48,8840 : 41,0815 39,9687 40,0002 40,0002 : 40,0002 40,0002 39,9687	0,0000 0,0000  0,0000 0,0000 0,0000  0,0000 0,0000 0,0000	-12,3447 -13,4473 : -21,1767 -22,2828 -22,2204 -23,3177 : -30,9988 -32,0961 -32,0337
Axial section	CD	50,0001 48,8840 : 41,0815 39,9687 40,0002 40,0002 : 40,0002 40,0002 39,9687	0,0000 0,0000  0,0000 0,0000 0,0000  0,0000 0,0000 0,0000	-12,3447 -13,4473 : -21,1767 -22,2828 -22,2204 -23,3177 : -30,9988 -32,0961 -32,0337

# 5. Shaping tool's profiling for the generation of a ball thread

Based on the generating principles previously presented, is determined the form of the primary peripheral surface of the shaping tool for the generation of a ball thread.

In Figure 6, are presented the reference systems, the 3D model of the ball thread and the primary peripheral surface of the shaping tool, reciprocally enveloping with the ball thread.

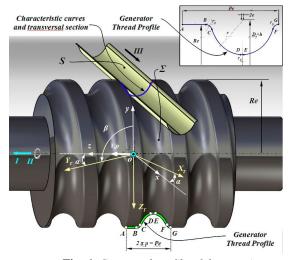


Fig. 6. Composed profile of the crossing section

In Figure 7 and Table 3, are presented the form and coordinates of the characteristic curve and of the crossing section.

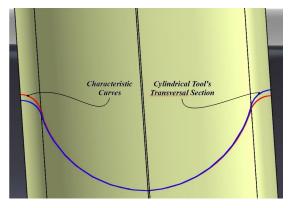


Fig. 7. Characteristic curve and crossing section

In Figure 8, it is presented the crossing section form of the cylindrical surface in the  $X_T Y_T Z_T$  reference system.

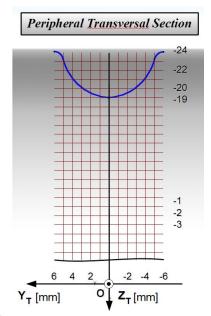


Fig. 8. Composed profile of the ball thread's crossing section

This reference system has the origin on the ball thread axis and the plane  $X_T Z_T$  perpendicular to the cylindrical surface's generatrix.

 Table 3. Coordinates of points from the characteristic

 curve and the crossing section of the shaping tool for

 the generation of a ball thread

the generation of a ball thread					
Profile	Crt. no.	X [mm]	Y [mm]	Z [mm]	
	1	-0,6388	23,9915	6,0911	
	2	-0,6382	23,9793	5,9358	
5	:	:	:	:	
rve	11	-0,3277	23,2586	5,0938	
Cu	:	:	:	÷.	
tic	20	-0,4954	19,2670	0,1007	
ris	21	-0,4993	19,2666	0,0934	
Characteristic Curves	:	:	:	:	
ara	30	-0,5308	19,2660	0,0349	
Ch	31	-0,6036	19,3451	-0,7176	
•	÷.	:	;		
	149	-0,6391	23,9793	-5,8002	
	150	-0,6391	23,9915	-5,9555	
Profile		X <sub>T</sub> [mm]	Y <sub>T</sub> [mm]	Z <sub>T</sub> [mm]	
1	1	0	-5,9894	-23,9833	
100	2	0	-5,8450	-23,9731	
al 1	· · ·		÷.	÷.	
ric	11	0	-5,0266	-23,2451	
pu	· · .	:		2	
Jyli (	20	0	-0,0213	-19,2733	
fC	21	0	-0,0136	-19,2731	
Axial Section of Cylindrical Tool	· · ·			:	
tio	30	0	0,0402	-19,2733	
Sec	31	0	0,0479	-19,2735	
al ,	:	:	:		
xi	149	0	5,8430	-24,0055	
$\mathbf{A}$	150	0	5,9897	-24,0169	

# 6. Shaping tool's profiling for the generation of a cycloid hub

In Figure 9, it is presented the cycloid worm with two starts, which has as generatrix in the frontal plane the epicycloids generated by a point from the roulette with radius r, rolling onto the base with radius R.

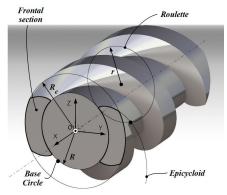
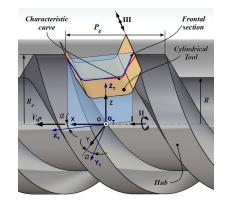


Fig. 9. The cycloid worm with two starts

In Figure 10, they are presented the cylindrical surface reciprocally enveloping with the cycloid worm, the characteristic curve and the crossing section of the composed cylindrical surface (surface generated by the shaping tool, in the rectilinear movement, III).



**Fig. 10.** The cylindrical surface, the characteristic curve and the crossing section

In Table 4 and Figure 11, are presented the coordinates and the form of the crossing section of cylindrical surface (the profile of the shaping tool).

### 7. Conclusions

The proposed method allows for the easy profiling of the generating tool for helical surface, determining in graphical and numerical form the characteristic curve and the axial section. The presented examples for the profiling of the helical surface as: trapezoidal thread, ball thread and cycloid hub, prove the capability of this method to approach a wider problem. Moreover the presented helical surfaces are composed surfaces, and in some situations are possible to highlight problems due to the presence of singular points, for which are given profiling solutions for shaping tool.

**Table 4.** Coordinates of points from the characteristic

 curve and the crossing section of the shaping tool for

 the generation of a trapezoidal thread

Profile	Crt. no.	X [mm]	Y [mm]	Z [mm]
	1	8,6607	0,0662	14,9999
	2	7,9821	0,5452	14,3732
	÷.		÷.	÷.
sə4.	11	4,3759	0,4975	10,0414
Cur	:	:	:	:
ic (	20	-1,5605	-0,0083	10,0000
rist	21	-2,6010	-0,0138	10,0000
Characteristic Curves	:	:	:	:
ara	30	-4,6530	-3,1375	11,3306
Ch	31	-5,3119	-2,5993	11,9297
	· · .			
	149	-7,9820	-0,5453	14,3731
	150	-8,6607	-0,0662	14,9999
Profile		$X_T[mm]$	Y <sub>T</sub> [mm]	$Z_T[mm]$
	1	-7,6818	0,0000	14,9999
100	2	-7,3141	0,0000	14,3856
L L	<i>:</i>	;	÷.	
ica	11	-3,2218	0,0000	10,0000
ndr	÷.	<i>:</i>		
yli	20	1,0739	0,0000	10,0000
J C	21	1,7899	0,0000	10,0000
n c	:	:	:	:
ctio	30	5,5486	0,0000	11,2717
Axial Section of Cylindrical Tool	31	5,8934	0,0000	11,8987
ial	:	:	:	:
Ax	149	7,3142	0,0000	14,3857
	150	7,6818	0,0000	14,9999

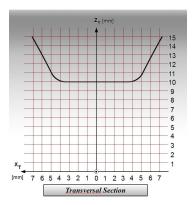


Fig. 11. The crossing section of the shaping tool

The method may highlight very accurate by the problems linked to the discontinuities emerged due to the singular points from the profiles.

The method is intuitive and very easy to apply.

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#### Metodă 3D pentru profilarea sculelor cilindrice generatoare a suprafețelor elicoidale

#### -Rezumat-

În prezenta lucrare, se propune o metoda grafică pentru profilarea sculelor cilindrice (scule de rabotat sau mortezat) destinate generării suprafețelor elicoidale de pas constant. Metoda, dezvoltată în mediul de proiectare CATIA, este bazată pe descompunerea mişcării elicoidale într-un ansamblu de mişcări echivalente, respectiv mişcări de rotație și translație.

A fost elaborată o aplicație soft dedicată, ce permite modelarea suprafeței elicoidale, determinarea curbei caracteristice și a secțiunii transversale a suprafeței cilindrice, reciproc înfășurătoare cu suprafața elicoidală. Sunt prezentate aplicații referitoare la generarea suprafețelor elicoidale de tip filet trapezoidal și filet pentru șurub cu bile.